

Shocks in plasma

"Shock" - shocked by an unexpected event

"Shock wave" - sudden transition in the properties of a fluid medium involving a difference in flow velocity across a narrow (ideally abrupt) transition

→ in physics: shock wave is a disturbance travelling at speed greater than the local sound speed

$$\Rightarrow \text{i.e. Mach number: } M = \frac{u_u}{c_s} > 1$$

in plasma physics we use the Alfvén speed:

$$M = \frac{u_u}{V_A} > 1$$

→ abrupt change in conditions: $P, \rho, T, \dots$

→ shock → carries energy forward @ shock velocity $> c_s$

→ heats & accelerates medium as it passes

→ shock heats the fluid behind it so the motion of the shockwave to the heated fluid is subsonic

i.e. changes in source of Energy are

communicated to the shock at a new

(higher) sound speed!

→ produces irreversible change in fluid state

(increase in entropy)

Rankine-Hugoniot relations

- first consider jump conditions with no B-field
- assume adiabatic shock
- in frame of the shock (i.e. shock front stationary), upstream fluid stationary
 - ↳ shock at $x=0$
- conservation laws: (remember lecture 5)

continuity equation: $\frac{d\rho}{dt} + \nabla(\rho \underline{u}) = 0$

momentum equation: $\rho \frac{d\underline{u}}{dt} + \nabla \rho \underline{u} \cdot \underline{u} + \nabla P = 0$
(no Lorentz force)

energy equation:

$\frac{d}{dt} \left(\frac{\rho u^2}{2} + \rho \epsilon \right) + \nabla \left[\rho \underline{u} \left(\epsilon + \frac{u^2}{2} \right) + P \underline{u} \right] = 0$
internal energy

→ also known as Euler equations

→ express the Euler equations in the form of: $\frac{d}{dt} \rho_Q = - \frac{d}{dx} \Pi_Q$

for ∞ -small interval $[x_1, x_2] \rightarrow \int_{x_1}^{x_2} \frac{d}{dt} \rho_Q dx \rightarrow 0$
assume steady state

→ apply logic + the divergence theorem:

$\iiint_V \nabla \underline{A} \cdot d\underline{V} = \oint_S \underline{A} \cdot d\underline{S}$
↑ volumetric change in A ↑ flux

→ rewrite the Euler equations in a "conservative form":

$$\frac{\partial}{\partial t} \rho_Q + \nabla \cdot \vec{T}_Q = S_Q$$

$\uparrow$ change in density of quantity Q
 $\uparrow$ flux of the quantity Q [per unit area per time] → flux
 $\nwarrow$ volumetric source of quantity Q

→ integrate the conservative form over some volume with a surface G and Apply the divergence theorem:

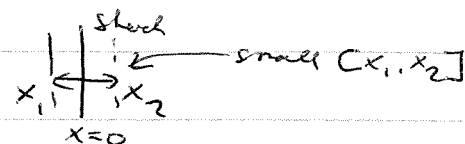
$$\int_V \nabla \cdot \vec{T}_Q \cdot dV = \oint_G \vec{T}_Q \cdot d\vec{A}$$

$$\Rightarrow \int_V \frac{\partial}{\partial t} \rho_Q + \oint_G \vec{T}_Q \cdot d\vec{A} = \text{net source in volume}$$

$$\Rightarrow \frac{\partial}{\partial t} Q + \oint_G \vec{T}_Q \cdot d\vec{A} = \text{net source in volume} = 0$$

$\uparrow$
 net flow of Q thgh surface G

→ we have form:



$$\int_{x_1}^{x_2} \frac{\partial}{\partial t} \rho_Q dx = - \int_{x_1}^{x_2} \frac{\partial}{\partial x} T_Q(x) dx = T_Q(x_2) - T_Q(x_1)$$

$= 0$

$\uparrow$
 approaches 0

for small $[x_1, x_2]$

or say steady state $\frac{\partial}{\partial t} = 0$

→ rewrite the continuity eq. as:

$$\begin{array}{ccc} \rho_u u_u & = & \rho_d u_d \\ \uparrow & & \uparrow \\ \text{upstream} & & \text{downstream} \end{array}$$

→ momentum equation:

$$\rho u_u^2 + P_u = \rho u_d^2 + P_d$$

→ energy equation:

$$u_u \left(\frac{1}{2} u_u^2 + \epsilon_u + \frac{P_u}{\rho_u} \right) = u_d \left(\frac{1}{2} u_d^2 + \epsilon_d + \frac{P_d}{\rho_d} \right)$$

→ and for ideal gas: $\epsilon = \frac{1}{\gamma-1} \cdot \frac{P}{\rho}$

$$\text{Substitute } \Rightarrow u_u \left(\frac{1}{2} u_u^2 + \frac{\gamma}{\gamma-1} \cdot \frac{P_u}{\rho_u} \right) = u_d \left(\frac{1}{2} u_d^2 + \frac{\gamma}{\gamma-1} \cdot \frac{P_d}{\rho_d} \right)$$

$$\Rightarrow \rho_u u_u \left(\epsilon_u + \frac{u_u^2}{2} \right) + P_u u_u = \rho_d u_d \left(\epsilon_d + \frac{u_d^2}{2} \right) + P_d u_d //$$

→ post shock (or particle) velocity u_p : (also piston)

$$u_p = u_u - u_d \quad \Rightarrow \quad u_d = u_u - u_p$$

→ continuity equation:

$$\Rightarrow \rho_u u_u = \rho_d (u_u - u_p)$$

$$\Rightarrow \frac{\rho_d}{\rho_u} = \frac{u_u}{u_u - u_p} // \quad \Rightarrow \rho_d = \frac{u_u \rho_u}{u_u - u_p} //$$

→ momentum equation:

$$P_d - P_u = \rho_u u_u^2 - \rho_d u_d^2$$

$$= \rho_u u_u^2 - \rho_d (u_u - u_p)^2$$

$$= \rho_u u_u^2 - \frac{u_u \rho_u}{u_u - u_p} (u_u - u_p)^2$$

as $\rho_d = \frac{u_u \rho_u}{u_u - u_p}$

$$\Rightarrow P_d - P_u = \cancel{\rho_u u_u^2} - \cancel{\rho_u u_u^2} + \rho_u u_u u_p$$

$$= \rho_u u_u u_p //$$

→ energy equation:

as $P_u \rightarrow 0$

$$u_d = u_u - u_p$$

$$\rho_u u_u \left(E_u + \frac{u_u^2}{2} \right) + \cancel{\rho_u u_u} = \rho_d u_d \left(E_d + \frac{u_d^2}{2} \right) + \rho_d u_d$$

$$\rho_u u_u E_u + \rho_u u_u \cdot \frac{u_u^2}{2} = \frac{u_u \rho_u}{u_u - u_p} \cdot (u_u - u_p) \cdot E_d$$

$$+ \frac{u_u \rho_u}{u_u - u_p} \cdot (u_u - u_p) \cdot \frac{(u_u - u_p)^2}{2} + \rho_d (u_u - u_p)$$

$$\rho_u u_u E_u + \cancel{\rho_u u_u \cdot \frac{u_u^2}{2}} = \rho_u u_u E_d + \cancel{\rho_u u_u \cdot \frac{u_u^2}{2}} - \rho_u u_u \cdot \frac{2 u_u u_p}{2}$$

$$+ \rho_u u_u \frac{u_p^2}{2} + \rho_d (u_u - u_p)$$

$$= u_u (P_d - P_u)$$

$$\Rightarrow \frac{1}{2} \rho_u u_u u_p^2 + \rho_u u_u (E_d - E_u) = \rho_u u_u^2 u_p + P_d u_p - P_d u_u$$

$$= \cancel{P_d u_u} - \cancel{P_d u_u} + P_d u_p$$

→ initial conditions ρ_0, P_0, ϵ_0 (before shock arrives)

$\Rightarrow \rho_u = \rho_0 \rightarrow$ initial density

$\Rightarrow \rho_d = \rho \rightarrow$ final shocked density

$\Rightarrow u_u = u_s \rightarrow$ shock velocity (we work in the frame of the shock)

$\Rightarrow P_u = P_0 = 0 \rightarrow$ pre-shock pressure is negligible in comparison

$\Rightarrow P_d = P \rightarrow$ shock pressure

$\Rightarrow$ rewrite R-H relations:

$$\rho_0 u_s = \rho (u_s - u_p)$$

$$P - P_0 = \rho_0 u_s u_p = P$$

$$P u_p = \frac{1}{2} \rho_0 u_s u_p^2 + \rho_0 u_s (\epsilon - \epsilon_0)$$

$\Rightarrow$ measure: u_s and u_p (if use flyer plate)

$\Rightarrow$ know: ρ_0 (initial conditions)

$\Rightarrow$ determine: P, ρ, ϵ (and ϵ_0)

Rankine-Hugoniot relations with B-field

→ Conserved parameters: mass, momentum, energy
AND E and B fields
(across the shock boundary)

→ since notation gets more complicated, use the form:

$$[X] = X_u - X_d \text{ for the conservation laws}$$

→ Shock geometry becomes important, define the angle of the upstream B-field to the shock normal as θ_{Bn}

- // - shock : $\theta_{Bn} = 0^\circ$
- $\perp$ - shock : $\theta_{Bn} = 90^\circ$
- oblique shock : $0^\circ < \theta_{Bn} < 90^\circ$
- quasi-// shock : $\theta_{Bn} < 45^\circ$
- quasi- $\perp$ shock : $\theta_{Bn} > 45^\circ$

→ mass conservation: the same as before, from continuity eq.:
(in the shock-normal direction)

$$\rho_u u_{un} = \rho_d u_{dn} \Rightarrow [\rho u_n] = 0$$

$$\Rightarrow \text{shock compression ratio : } r = \frac{\rho_d}{\rho_u} > 1$$

maximum value of r can be determined
from the conservation laws (see later)

→ E & B field conservation:

first consider changes associated with the fluid flow

→ assume a flat shock and position far away from any turbulence $\Rightarrow$ current can be neglected

$$\text{Ohm's Law: } \underline{j} = \sigma (\underline{E} + \underline{u} \times \underline{B})$$

$$\text{Faraday's Law: } \frac{\partial \underline{B}}{\partial t} = -\nabla \times \underline{E} = 0 \quad \leftarrow \text{(have steady state)}$$

$$\Rightarrow \underline{E} = -\underline{u} \times \underline{B}$$

i.e. in a perfectly conducting fluid in a co-moving frame, the induced electric field is:

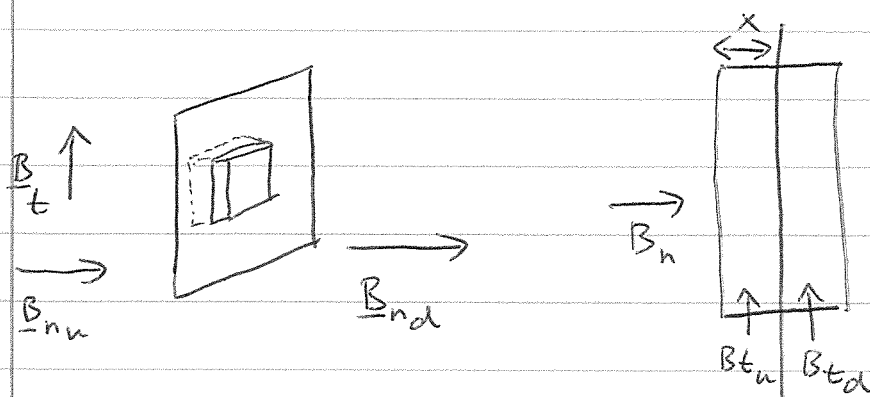
$$\underline{E}' = \underline{E} + \underline{u} \times \underline{B} = 0 \quad (\text{vanishes})$$

$\Rightarrow$ thus the conservation of the magnetic flux (Faraday's law) gives: $\hat{n} \times (\underline{u} \times \underline{B})$ conserved across the boundary:

$$[\underbrace{u_n B_t - B_n u_t}_{\text{i.e. perpendicular}}] = 0$$

$\uparrow \quad \quad \uparrow$
normal transverse

→ B-field conserved: the same flux in/out



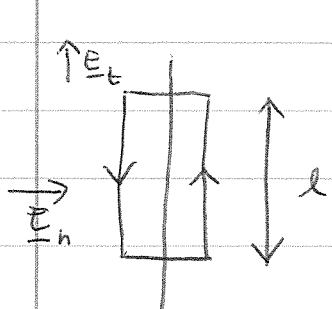
→ the divergence theorem: $\iiint_V \nabla \cdot \underline{B} \cdot dV = \oint \underline{B} \cdot dS$

and $\nabla \cdot \underline{B} = 0$

$\Rightarrow B_{nu} = B_{nd} \Rightarrow [\underline{B}_n] = 0$

→ B_t is the same $\Rightarrow$ cancels out

→ E-field conservation:



from Faraday's Law $\frac{\partial B}{\partial t} = -\nabla \times \underline{E} = 0$ steady state

$\oint \underline{E} \cdot d\ell = \int \nabla \times \underline{E} \cdot dS = 0$

$\Rightarrow E_t$ continuous $\Rightarrow l E_{tu} = l E_{td}$

$\Rightarrow [\underline{E}_t] = 0$

→ $\underline{E} = -\underline{u} \times \underline{B} \Rightarrow [u_n B_t - B_n u_t] = 0$

→ momentum conservation.

$$\underline{F} = m \cdot \underline{a}$$

• || to the shock normal: (normal)

$$\rightarrow \underbrace{\rho_u u_{u_n} \cdot \underline{u}_{u_n}}_{\text{mass flux!}} - \rho_d u_{d_n} \cdot \underline{u}_{d_n} = m \cdot \underline{a}_n$$

per time, per area

→ kinetic pressure (force per area)

$$P_d - P_u$$

→ magnetic pressure: $\frac{B_{tu}^2}{2\mu_0} - \frac{B_{td}^2}{2\mu_0}$ (only normal direction)

and from lecture 5 we had momentum equation:

$$\rho \left[\frac{\partial \underline{u}}{\partial t} + (\underline{u} \cdot \nabla) \underline{u} \right] = \underline{j} \times \underline{B} - \nabla P + \underline{F} \Rightarrow [\rho u^2 + P] = 0$$

→ integrating and taking both pressure components:
we get the conservation of the momentum flux
normal to the shock:

$$\left[\rho u_n^2 + P + \frac{B_t^2}{2\mu_0} \right] = 0$$

• ⊥ to the shock normal (transverse)

→ momentum conservation across the shock:

$$\rho_u u_{ut} \frac{u}{u_t} - \rho_d u_{dt} \frac{u}{u_t} = m \cdot a_t$$

→ no pressure difference in the transverse direction (thermal, kinetic)

→ no change in B-pressure: $B_n = \text{const.}$

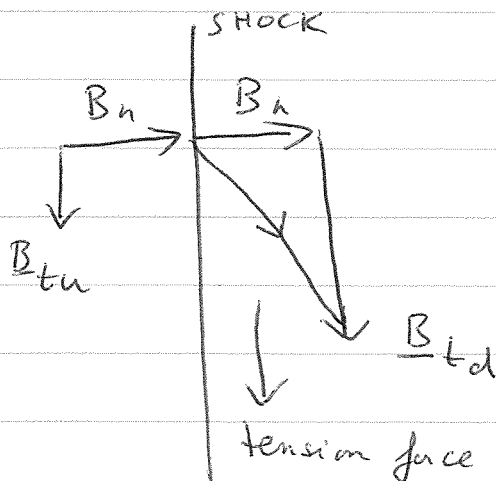
→ but must account for magnetic tension force:

$$\frac{1}{\mu_0} (\underline{B} \cdot \nabla) \underline{B} \Rightarrow \frac{B_n B_{tu} - B_n B_{td}}{\mu_0}$$

→ plug into the momentum equation in the form of:

$$[\rho u^2 + P] = 0$$

$$\Rightarrow \left[\rho u_t^2 + \frac{B_n B_t}{\mu_0} \right] = 0$$



→ energy conservation with B-field

- include kinetic, internal energy, work done ($\Rightarrow$ enthalpy)
and the EM radiation (Poynting vector).

$\Rightarrow$ kinetic energy: $E_k = \frac{1}{2} \rho_u u_n u_n^2 = \frac{1}{2} \rho u_{nd} u_{nd}^2$

$\Rightarrow$ internal energy: $E = \frac{\alpha}{2} k_B T$ and for ideal gas: $PV = n k_B T$

$$\Rightarrow \frac{P}{\rho} = k_B T \Rightarrow E = \frac{\alpha}{2} \cdot \frac{P}{\rho} = \frac{1}{\gamma-1} \cdot \frac{P}{\rho}$$

$\rightarrow$ work done: $W = PdV = \left[\frac{P}{\rho} \right]$

$\rightarrow$ enthalpy: $E + pdV = E + \frac{P}{\rho} = \frac{\gamma}{\gamma-1} \cdot \frac{P}{\rho}$ (remember lecture 8)

monatomic ideal gas: $\gamma = \frac{c_p}{c_v} = \frac{\alpha+2}{\alpha} = \frac{5}{3}$ (adiabatic)

$$\Rightarrow \frac{\gamma-1+1}{\gamma-1} = \frac{\gamma}{\gamma-1}$$

$$\Rightarrow H = E + \frac{P}{\rho} = \frac{1}{\gamma-1} \cdot \frac{P}{\rho} + \frac{P}{\rho} = \frac{\gamma}{\gamma-1} \cdot \frac{P}{\rho} //$$

$\rightarrow$ the Poynting flux: $\underline{S} = \frac{\underline{E} \times \underline{B}}{\mu_0}$

and since $\underline{E} = \underline{u} \times \underline{B} \Rightarrow \underline{S} = \frac{(\underline{u} \times \underline{B}) \times \underline{B}}{\mu_0}$

using the vector identity: $\underline{A} \times \underline{B} \times \underline{B} = \underline{A} B^2 - (\underline{A} \cdot \underline{B}) \underline{B}$

$$\Rightarrow \underline{S} = \frac{\underline{u} B^2}{\mu_0} - \frac{(\underline{u} \cdot \underline{B}) \underline{B}}{\mu_0}$$

$\Rightarrow$ thus the complete expression for the energy conservation across the shock front including the kinetic, internal and electromagnetic energy flux is:

$$\left[\rho u_n \left(\frac{1}{2} u^2 + \frac{r}{r-1} \frac{P}{\rho} \right) + u_n \frac{B^2}{\mu_0} - \underline{u} \cdot \underline{B} \frac{B_n}{\mu_0} \right] = 0$$

$\nwarrow$ mass flux

$\nearrow$ mag. pressure

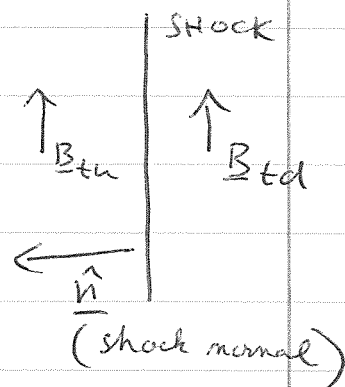
remember the energy equation (MHD):

$$\frac{d}{dt} \left(\frac{\rho u^2}{2} + \rho \epsilon \right) = -\nabla \cdot \left[\rho \underline{u} \left(\epsilon + \frac{u^2}{2} \right) + P \underline{u} \right]$$

$\Rightarrow$ solution for perpendicular shocks:

$$\underline{B} \perp \underline{n} \quad \text{and} \quad \underline{u} \parallel \underline{n}$$

$\rightarrow$ magnetic field lines compressed by the same factor as density



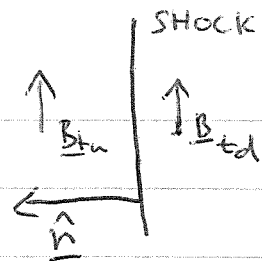
$$[B_n] = 0, B_{nu} = 0 \Rightarrow B_{nd} = 0$$

$\rightarrow$ mass conservation: $\rho_u u_{nu} = \rho_d u_{nd}$

$$\Rightarrow r = \frac{\rho_d}{\rho_u} = \frac{u_{nu}}{u_{nd}}$$

for transverse shock then: $\left[\rho u_n u_t - \frac{B_n}{\mu_0} \cdot \overbrace{B_t}^{=0} \right] = 0$

Solutions for $\perp$ shocks ($\underline{B} \perp \hat{n}$)
($\underline{u} \parallel \hat{n}$)



→ momentum conservation:

$$\rho_u u_u^2 + P_u + \frac{B_u^2}{2\mu_0} = \rho_d u_d^2 + P_d + \frac{B_d^2}{2\mu_0}$$

and $\rho_d = r \cdot \rho_u$, $u_d = \frac{u_u}{r}$, $B_d = r \cdot B_u$

→ substitute:

as: $r = \frac{\rho_d}{\rho_u} = \frac{u_u}{u_d}$

$$\rho_u u_u^2 + P_u + \frac{B_u^2}{2\mu_0} = \rho_u \cdot r \cdot \left(\frac{u_u}{r}\right)^2 + \frac{r^2 B_u^2}{2\mu_0} + P_d$$

$$\Rightarrow \rho_u u_u^2 \left(1 - \frac{1}{r}\right) + (P_u - P_d) + \frac{B_u^2}{2\mu_0} (1 - r^2) = 0 //$$

→ energy conservation: $\theta_{Bn} = 90^\circ \Rightarrow$ (no $\parallel$ B-field component)
both $B_{nd} = 0$
 $B_{nu} = 0 //$ 0

$$\begin{aligned} \rho_u u_u \left(\frac{1}{2} u_u^2 + \frac{r}{r-1} \cdot \frac{P_u}{\rho_u} \right) + u_u \frac{B_u^2}{\mu_0} - \cancel{u \cdot B} \frac{\cancel{B_n}}{\mu_0} \\ = \rho_d u_d \left(\frac{1}{2} u_d^2 + \frac{r}{r-1} \cdot \frac{P_d}{\rho_d} \right) + u_d \frac{B_d^2}{\mu_0} - \cancel{\phi} \\ = \cancel{\rho_u \cdot r \cdot \frac{u_u}{r}} \left(\frac{1}{2} \cdot \frac{u_u^2}{r^2} + \frac{r}{r-1} \cdot \frac{P_d}{\rho_u \cdot r} \right) + \cancel{\frac{u_u}{r}} \frac{r^2 B_u^2}{2\mu_0} \end{aligned}$$

$$\Rightarrow \frac{1}{2} \rho_u u_u^{\cancel{2}} \frac{u_u^2}{r^2} + \left(\frac{r}{r-1} \right) \cancel{u_u} \cdot P_u + \cancel{u_u} \frac{B_u^2}{\mu_0}$$

$$= \frac{1}{2} \rho_u \frac{u_u^{\cancel{2}} u_u^2}{r^2} + \left(\frac{r}{r-1} \right) \cancel{u_u} \cdot \frac{P_d}{r} + \frac{\cancel{u_u} \cdot r B_u^2}{\mu_0}$$

$$\Rightarrow \frac{1}{2} \rho_u u_u^2 \left(1 - \frac{1}{r^2}\right) + \frac{\gamma}{\gamma-1} \left(P_u - \frac{P_d}{r}\right) + \frac{B_u^2}{\mu_0} (1-r) = 0$$

$\rightarrow$ eliminate P_d by substitution:

$$P_d = \rho_u u_u^2 \left(1 - \frac{1}{r}\right) + P_u + \frac{B_u^2}{2\mu_0} (1-r^2)$$

$$\Rightarrow \frac{1}{2} \rho_u u_u^2 \left(1 - \frac{1}{r^2}\right) + \frac{\gamma}{\gamma-1} \left(P_u - \frac{\rho_u u_u^2 \left(1 - \frac{1}{r}\right) + P_u + \frac{B_u^2}{2\mu_0} (1-r^2)}{r}\right) - \frac{P_u}{r} - \frac{B_u^2}{2\mu_0} \frac{(1-r^2)}{r} + \frac{B_u^2}{\mu_0} (1-r) = 0$$

$/ \times r$

$$\frac{1}{2} \rho_u u_u^2 \left(r - \frac{1}{r}\right) + \frac{\gamma}{\gamma-1} \left(r P_u - \rho_u u_u^2 \left(1 - \frac{1}{r}\right) - P_u - \frac{B_u^2}{2\mu_0} (1-r^2)\right) + r \frac{B_u^2}{\mu_0} (1-r) = 0$$

$/ \times \rho_u u_u^2$

$$\frac{1}{2} \left(r - \frac{1}{r}\right) + \frac{\gamma}{\gamma-1} \left(r \frac{P_u}{\rho_u u_u^2} - \frac{P_u}{u_u^2 \rho_u} - \left(1 - \frac{1}{r}\right) - \frac{B_u^2}{2\mu_0} \frac{(1-r^2)}{\rho_u u_u^2}\right) + \frac{r B_u^2}{\rho_u u_u^2 \mu_0} (1-r) = 0$$

$/ \times 2(\gamma-1)$

$$(\gamma-1) \left(r - \frac{1}{r}\right) + 2\gamma \frac{P_u}{u_u^2 \rho_u} (r-1) - 2\gamma \left(1 - \frac{1}{r}\right) - \frac{2\gamma B_u^2}{u_u^2 \mu_0 \rho_u} (1-r^2) + \frac{2r B_u^2}{u_u^2 \mu_0 \rho_u} (1-r)(\gamma-1) = 0$$

$/ \times r$

$$\stackrel{=(r-1)(r+1)}{(\gamma-1)(r^2-1)} + \frac{2\gamma r P_u}{u_u^2 \rho_u} (r-1) - 2\gamma (r-1) + \frac{\gamma B_u^2}{\mu_0 \rho_u u_u^2} r (r^2-1) + \frac{2r^2 B_u^2}{u_u^2 \mu_0 \rho_u} (1-r)(\gamma-1) = 0$$

$$\Rightarrow (r-1) \left[(r-1)(r+1) + r \frac{2\gamma P_u}{u_u^2 \rho_u} - 2\gamma + \frac{\gamma B_u^2}{u_u^2 \mu_0 \rho_u} \cdot r (r+1) - r^2 \frac{2B_u^2}{u_u^2 \mu_0 \rho_u} (\gamma-1) \right] = 0$$

$$\Rightarrow (r-1) \left[r^2 \frac{\gamma B_u^2}{u_u^2 \mu_0 \rho_u} - r^2 \frac{2\gamma B_u^2}{u_u^2 \mu_0 \rho_u} + r^2 \frac{2B_u^2}{u_u^2 \mu_0 \rho_u} + r \frac{2\gamma P_u}{u_u^2 \rho_u} + r \frac{\gamma B_u^2}{u_u^2 \mu_0 \rho_u} + r(\gamma-1) + \gamma - 1 - 2\gamma \right] = 0$$

$$\Rightarrow (r-1) \left[r^2 \frac{(2-\gamma) B u^2}{u_u^2 \rho_u P_u} + r \left(\frac{\gamma B u^2}{u_u^2 \rho_u P_u} + \frac{2 \gamma P_u}{u_u^2 \rho_u} + (\gamma-1) \right) - (\gamma+1) \right] = 0$$

$\Rightarrow$ for strong shocks at high velocities the Mach number $M \rightarrow \infty$ and $u_u \rightarrow \infty$, thus the approximation can be made: $\frac{1}{u_u^2}$ terms $\rightarrow 0$

$$\Rightarrow (r-1) [r^2 \cdot 0 + r(0+0+\gamma-1) - (\gamma+1)] = 0$$

$$\Rightarrow (r-1) [r(\gamma-1) - (\gamma+1)] = 0$$

$\rightarrow$ 2 solutions: (1) $r=1 \Rightarrow$ not a shock
(not a solution)

$$(2) r(\gamma-1) - (\gamma+1) = 0$$

$$\Rightarrow r = \frac{\gamma+1}{\gamma-1} \text{ and for ideal gas } \gamma = 5/3$$

$$\Rightarrow r = \frac{5/3 + 3/3}{5/3 - 3/3} = 4 //$$

i.e. the maximum compression ratio

$$r = \frac{\rho_d}{\rho_u} = \frac{u_{du}}{u_{ud}} = 4 //$$

Solution for $\parallel$ shocks ($\underline{B} \parallel \underline{\hat{n}}$)

→ i.e. no $\perp$ B-field component, $B_t = 0$ ($\theta_{Bn} = 90^\circ$)

⇒ B-field does not change across the shock

⇒ particles can move along B-field lines upstream into the shock

⇒ simple hydrodynamic shock

Collisionless shocks

→ bulk behaviour by interactions of charged particles via EM fields

⇒ particles can travel against the bulk flow

⇒ non-linear interactions upstream

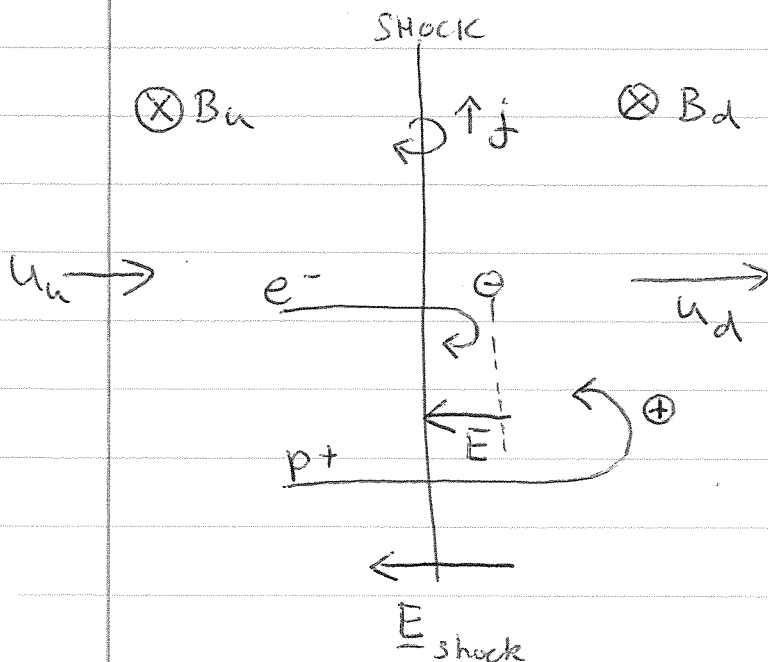
→ for $\perp$ collisionless shock:

• $e^- \rightarrow$ small gyro-radius

• change in $B_t \Rightarrow$ current layer $\mathcal{J}$

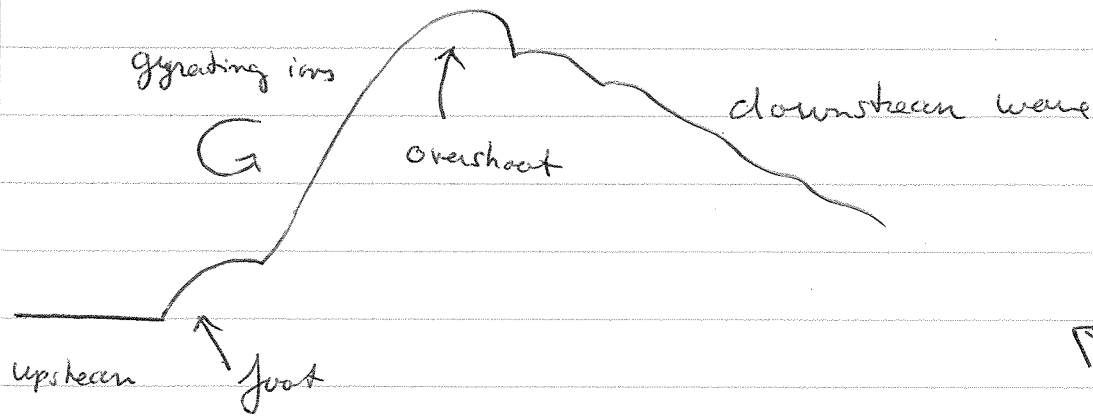
$$\nabla \times \underline{B} = \mu_0 \underline{j}$$

• ions/electrons decelerated by E-field



• E-field induced due to different radius of gyration between electrons and ions/protons

(protons/ions gyrate further into the shock)



→ shock variability: particle reflection process unstable $\Rightarrow$ leads to ripples in shock front (shock reformation) and particle acceleration

→ particles escape upstream if α_{Bn} not too large $\Rightarrow$ fore shock created

- unstable generation of waves

- quasi- $\perp$ shock ($\alpha > 45^\circ$) - stable up-down stream transition
 - steep rise in B-field $\Rightarrow$ "ramp"

- quasi- $\parallel$ shock ($\alpha < 45^\circ$) - transition from up-stream to downstream is broad

(1-2 Earth radii for bow shock in Earth)

$\Rightarrow$ turbulent region

$\Rightarrow$ unsteady shock

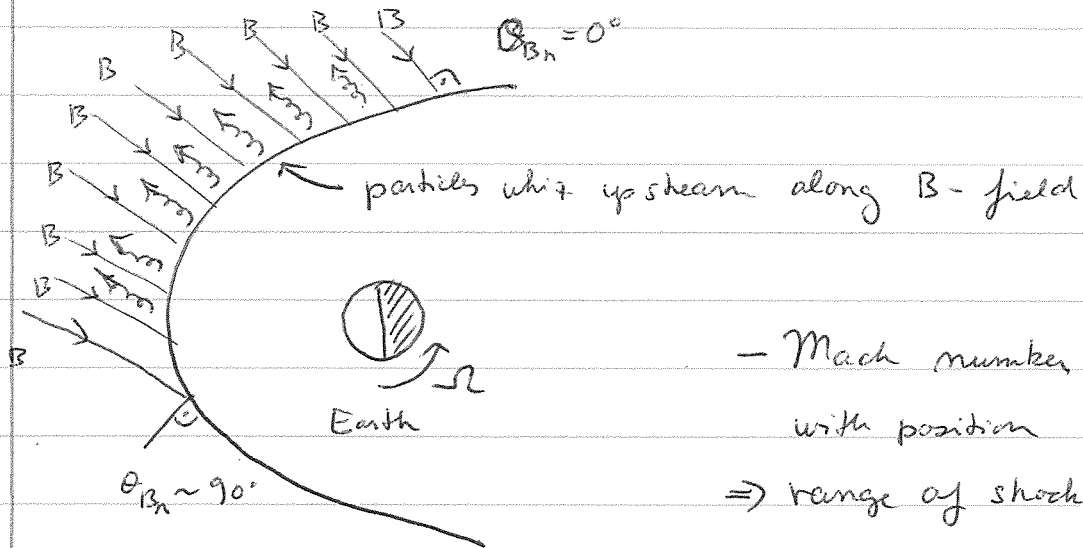
The Bow shock (example of a collisionless shock)

→ solar wind is super-Alfvénic
⇒ bow shock generated

⇒ generates magnetopause: boundary between the solar wind and Earth's magnetosphere

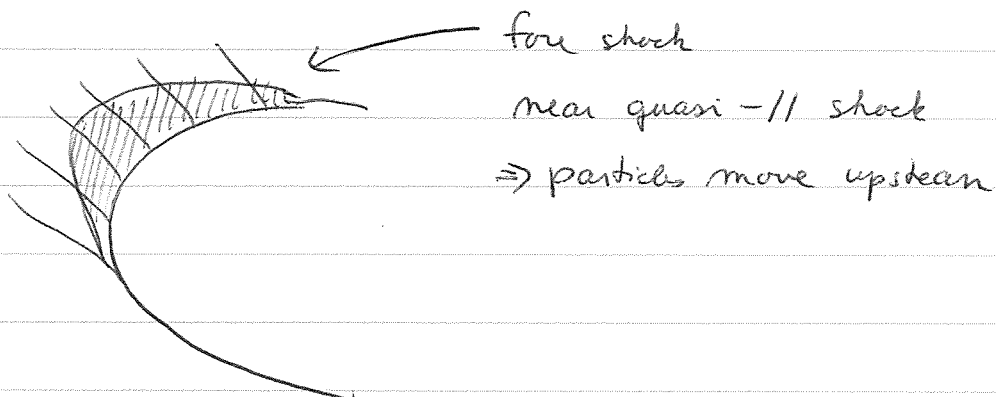
- solar wind pressure (components: ram, magnetic and plasma/thermal) compresses the Earth's B-field into cavity
- solar wind deflected around magnetosphere

→ magne to sheath = shocked, deflected solar wind



- Mach number varies with position

⇒ range of shock conditions



Radiative shocks

→ radiative relaxation layer, ahead of shock material is preheated generating a new set of conditions:

$$\rho_3, u_3, P_3, T_3 \text{ further downstream}$$

→ within the radiative relaxation layer the temperature drops and the gas is squeezed to higher density

→ to get the jump conditions for a radiative shock, we include the cooling term $L(p, T)$

→ for differential notation, the Euler equations are denoted as:

$$\text{continuity: } \frac{d}{dx} (\rho u) = 0$$

$$\text{momentum: } u \frac{du}{dx} = -\frac{1}{\rho} \frac{dP}{dx}$$

$$\text{energy: } \frac{d}{dx} (\rho \epsilon u) = \rho u \frac{d\epsilon}{dx} = -P \frac{du}{dx} - \rho L$$

$$\text{and for ideal gas: } \epsilon = \frac{1}{\gamma - 1} \cdot \frac{P}{\rho}$$

$$\Rightarrow \frac{d\epsilon}{dx} = \frac{1}{\gamma - 1} \left(\frac{1}{\rho} \frac{dP}{dx} - \frac{P}{\rho^2} \frac{d\rho}{dx} \right)$$

and we have $\frac{1}{\rho} \frac{dP}{dx} = -\frac{1}{u} \frac{du}{dx}$

since $\rho \propto \frac{1}{u}$

$$\Rightarrow \frac{u}{\gamma-1} \left(\frac{dP}{dx} + \frac{P}{u} \frac{du}{dx} \right) + P \frac{du}{dx} = -\rho L$$

substituting: $\frac{dP}{dx} = -\rho u \frac{du}{dx}$

$$\Rightarrow -\frac{\rho u^2}{\gamma-1} \frac{du}{dx} + \frac{\gamma}{\gamma-1} P \frac{du}{dx} = -\rho L$$

as $\frac{1}{\gamma-1} + \frac{\gamma-1}{\gamma-1} = \frac{\gamma}{\gamma-1}$

and speed of sound: $u_{ca}^2 = \frac{\gamma P}{\rho}$ (adiabatic)

$$\Rightarrow \text{thus: } \frac{u_{ca}^2 - u^2}{\gamma-1} \frac{du}{dx} = -L$$

Since post-shock flow is sub-sonic ($u < u_{ca}$) and $L > 0$
 we conclude $\frac{du}{dx} < 0$, so mass conservation
 implies $\frac{dP}{dx} > 0$

$\Rightarrow$ mass and momentum conservation apply as before:

$$\rho_3 u_3 = \rho_u u_u = \rho_d u_d$$

$$\rho_3 u_3^2 + P_3 = \rho_u u_u^2 + P_u = \rho_d u_d^2 + P_d$$

as u drops in the radiative relaxation layer

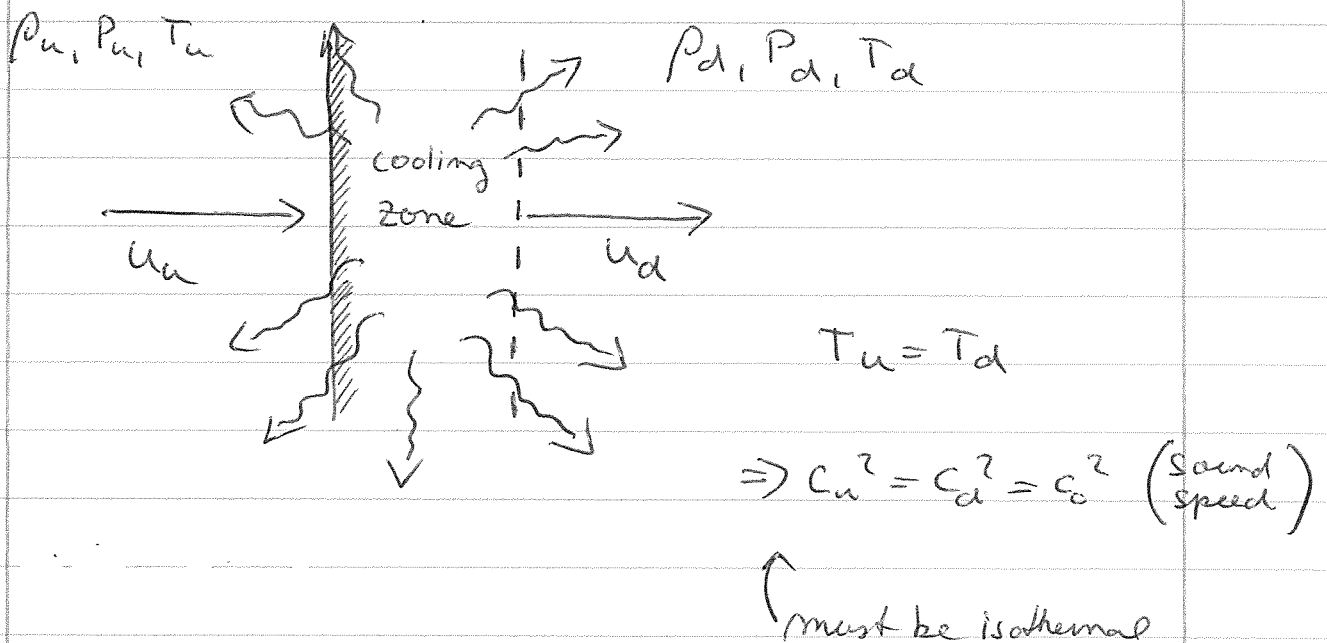
$$\rho u^2 = (\rho u) u \text{ drops}$$

and thus pressure must rise to compensate

→ i.e. pressure does not go down, thus the drop in temperature must come with a proportional rise in density to maintain the pressure

→ with efficient post shock cooling, we can get very high compression ratios
(remember the max $r=4$ for non-radiative shocks)

→ Special case: isothermal shock
(when have long cooling times or for balanced cooling/heating)



→ obtain new jump conditions

• Isothermal shocks: $T_u = T_d$

$$\text{and } c_{is} = \sqrt{\frac{P}{\rho}} = \sqrt{\frac{k_B T}{m}} \Rightarrow c_u^2 = c_d^2 = c_o^2$$

← (isothermal sound speed)

→ Speed of sound constant across the shock boundary:

$$c_o^2 = \frac{P_u}{\rho_u} = \frac{P_d}{\rho_d}$$

→ RH1: $\rho_u u_u = \rho_d u_d$

→ R-H2: $\rho_u u_u^2 + P_u = \rho_d u_d^2 + P_d$

Substitute for P
into RH-2

$$\Rightarrow \rho_u u_u^2 + \rho_u c_o^2 = \rho_d u_d^2 + \rho_d c_o^2 \quad / \div \rho_u$$

and for RH1 we have: $\frac{\rho_d}{\rho_u} = \frac{u_u}{u_d}$

$$\Rightarrow u_u^2 + c_o^2 = \frac{u_u}{u_d} u_d^2 + \frac{u_u}{u_d} c_o^2 \quad / \times u_d$$

$$\Rightarrow u_d u_u^2 + u_d c_o^2 + u_u u_d^2 + u_u c_o^2$$

$$\Rightarrow (u_d - u_u) c_o^2 = u_u u_d (u_d - u_u)$$

→ for $u_d \neq u_u \Rightarrow c_o^2 = u_u u_d$

$$\therefore u_d = \frac{c_o^2}{u_u} //$$

$$\Rightarrow \text{compression ratio: } r = \frac{\rho_d}{\rho_u} = \frac{u_u}{u_d} = \frac{u_u^2}{c_o^2} \equiv M_T^2 \quad (\text{Mach number})$$

can be arbitrarily high!